

CISTERN SIZING CALCULATIONS BY DRAINAGE AREAS:

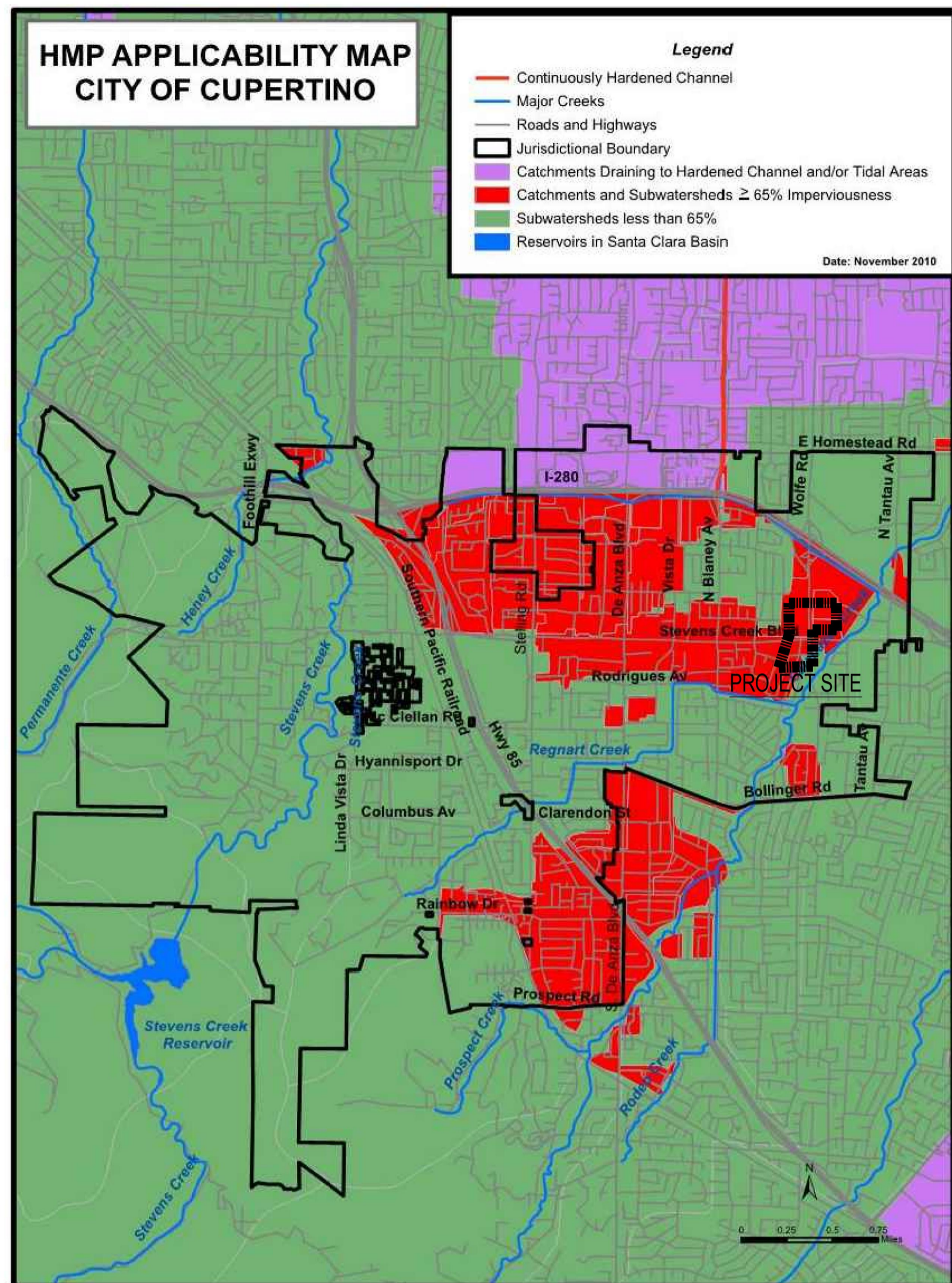
Approval Body: Director / Staff
 Approval Date: 06/03/22
 Signature: Jim Throop
 Case Manager

| Drainage Area 1 (DA-1) Volume Based Treatment Measures using the UROM Approach | | | |
|--|--|---------------------|---|
| Step 1. | Drainage Area for BMP: | 17.28 acres | |
| Step 2. a. | Impervious Area: | 10.60 acres | |
| | Impervious ratio: (i) | 61.4% | |
| Step 3. | Watershed runoff Coefficient Cw = | 0.419 | (Cw = 0.858i ³ -0.78i ² +0.774i+0.04) |
| Step 4. | Mean Annual Precipitation | 16 inches | |
| Step 5. | Closest Rain Gage San Jose Airport | | |
| | Gage | MAP _{gage} | (P _e) _{gage} (in) |
| | San Jose Airport | 13.9 | 0.512 |
| | Palo Alto | 13.7 | 0.522 |
| | Morgan Hill | 19.5 | 0.76 |
| MAP _{gage} | 13.9 | | |
| (P _e) _{gage} | 0.512 | | |
| Step 6. | Mean Storm Event Precipitation Depth (P _e) _{site} | 0.589 inches | (P _e) _{site} = (P _e) _{gage} X (MAP _{site})/(MAP _{gage}) |
| Step 7. | "a" regression constant | | |
| | a= 48 hour | 1.963 | a= 48 hour |
| | a= 24 hour | 1.582 | |
| | a= 12 hour | 1.312 | |
| Step 8. | Maximized Storage Area | | |
| | P _e = (a X Cw) X P _e | 0.485 inches | |
| Step 9. | Volume of Runoff to be Treated | | |
| | Design Volume = Po X A X 11/12in | 0.699 acre-ft | |
| Step 10. | Size Cistern | | |
| | Total Cistern Storage Volume | 30,439 cuft | |

| Drainage Area 2 (DA-2) Volume Based Treatment Measures using the UROM Approach | | | |
|--|--|---------------------|---|
| Step 1. | Drainage Area for BMP: | 32.05 acres | |
| Step 2. a. | Impervious Area: | 20.64 acres | |
| | Impervious ratio: (i) | 64.4% | |
| Step 3. | Watershed runoff Coefficient Cw = | 0.444 | (Cw = 0.858i ³ -0.78i ² +0.774i+0.04) |
| Step 4. | Mean Annual Precipitation | 16 inches | |
| Step 5. | Closest Rain Gage San Jose Airport | | |
| | Gage | MAP _{gage} | (P _e) _{gage} (in) |
| | San Jose Airport | 13.9 | 0.512 |
| | Palo Alto | 13.7 | 0.522 |
| | Morgan Hill | 19.5 | 0.76 |
| MAP _{gage} | 13.9 | | |
| (P _e) _{gage} | 0.512 | | |
| Step 6. | Mean Storm Event Precipitation Depth (P _e) _{site} | 0.589 inches | (P _e) _{site} = (P _e) _{gage} X (MAP _{site})/(MAP _{gage}) |
| Step 7. | "a" regression constant | | |
| | a= 48 hour | 1.963 | a= 48 hour |
| | a= 24 hour | 1.582 | |
| | a= 12 hour | 1.312 | |
| Step 8. | Maximized Storage Area | | |
| | P _e = (a X Cw) X P _e | 0.514 inches | |
| Step 9. | Volume of Runoff to be Treated | | |
| | Design Volume = Po X A X 11/12in | 1.372 acre-ft | |
| Step 10. | Size Cistern | | |
| | Total Cistern Storage Volume | 59,779 cuft | |

NOTE:

FOR THE PURPOSE OF THIS STORMWATER MANAGEMENT PLAN, THE SITE HAS BEEN LOOKED AT AS TWO DRAINAGE AREAS. RAINWATER CISTERNS WILL BE DESIGNED IN MORE DEPTH AND COORDINATED WITH THE PLUMBING ENGINEER TO WORK WITH CONSTRUCTION PHASING, THE SITE SPANNING PUBLIC RIGHT OF WAY AND IRRIGATION AND TOILET DEMANDS. THESE CISTERNS WILL BE SIZED INDIVIDUALLY BASED THEIR RESPECTIVE DRAINAGE AREAS.



HYDROMODIFICATION MAP

N.T.S.

NOTE:

PROJECT IS EXEMPT FROM HYDROMODIFICATION BECAUSE IT IS LOCATED IN A WATERSHED THAT IS GREATER THAN 65% IMPERVIOUS.

PRE AND POST DEVELOPMENT STORM DRAINAGE RUNOFF ANALYSIS:

CALCULATION OF WEIGHTED "C", C_w

The following equation is used to compute the weighted "c":

$$C_w = \frac{C_p A_p + C_i A_i + C_A}{A_T}$$

- C_w = Weighted runoff coefficient for drainage area A
- C_i = Impervious Area Runoff Coefficient (c varies, see below)
- C_p = Pervious Area Runoff coefficient (c varies, see below)

- A_i = Impervious Drainage Area (acres)
- A_p = Pervious Drainage Area (acres)
- A_T = Total Drainage Area (acres)

| Site Pre-Development Weighted "C" | | |
|-----------------------------------|-------------|----------|
| Pervious Area = | 0.87 ac | c = 0.30 |
| Impervious Area = | 49.95 ac | c = 0.90 |
| Total Area = | 50.82 ac | |
| C_{w(pre)} = | 0.89 | |

| Site Post-Development Weighted "C" | | |
|------------------------------------|-------------|----------|
| Landscape Area = | 15.20 ac | c = 0.30 |
| Impervious Area = | 34.14 ac | c = 0.90 |
| Total Area = | 49.33 ac | |
| C_{w(post)} = | 0.72 | |

CALCULATION OF RAINFALL INTENSITY, i

i = Intensity (in/hr) based on NOAA's PDS-based precipitation frequency estimates for Cupertino

TC = Time of Concentration (minutes), assumed to be 10 minutes

| Calculation of 10-Year Rainfall Intensity | | | |
|---|---------------|-----------------------------|---------------|
| TC _{pre} = | 10.00 minutes | TC _{post} = | 10.00 minutes |
| i _{10year(pre)} = | 1.76 in/hr | i _{10year(post)} = | 1.76 in/hr |

| Calculation of 25-Year Rainfall Intensity | | | |
|---|---------------|-----------------------------|---------------|
| TC _{pre} = | 10.00 minutes | TC _{post} = | 10.00 minutes |
| i _{25year(pre)} = | 2.14 in/hr | i _{25year(post)} = | 2.14 in/hr |

| Calculation of 100-Year Rainfall Intensity | | | |
|--|---------------|------------------------------|---------------|
| TC _{pre} = | 10.00 minutes | TC _{post} = | 10.00 minutes |
| i _{100year(pre)} = | 2.74 in/hr | i _{100year(post)} = | 2.74 in/hr |

CALCULATION OF 10-YEAR PEAK FLOW AND WATER QUALITY FLOW, Q

Use the Rational Equation for Peak Flow Calculation:
 $Q = C_w * i * A_T$

- Q = Peak Flow (cfs) for drainage area "A"
- C_w = Weighted runoff coefficient for drainage area A
- i = Intensity (in/hr) based on NOAA's PDS-based precipitation frequency estimates for Cupertino
- A_T = Total Drainage Area (acres)

| 10-Year Pre-Development Rainfall Peak Flow | | | |
|--|---------------------------|------------------|--|
| C _w = | 0.89 | | |
| i = | 1.8 in/hr | | |
| A _T = | 49.13 acres | | |
| Q_{pre-10year} = | 0.89 * 1.8 * 49.13 | 76.93 cfs | |

| 10-Year Post-Development Rainfall Peak Flow | | | |
|---|---------------------------|------------------|--|
| C _w = | 0.72 | | |
| i = | 1.8 in/hr | | |
| A _T = | 49.13 acres | | |
| Q_{post-10year} = | 0.72 * 1.8 * 49.13 | 61.84 cfs | |

CALCULATION OF 25-YEAR PEAK FLOW AND WATER QUALITY FLOW, Q

Use the Rational Equation for Peak Flow Calculation:
 $Q = C_w * i * A_T$

- Q = Peak Flow (cfs) for drainage area "A"
- C_w = Weighted runoff coefficient for drainage area A
- i = Intensity (in/hr) based on NOAA's PDS-based precipitation frequency estimates for Cupertino
- A_T = Total Drainage Area (acres)

| 25-Year Pre-Development Rainfall Peak Flow | | | |
|--|---------------------------|------------------|--|
| C _w = | 0.89 | | |
| i = | 2.1 in/hr | | |
| A _T = | 49.13 acres | | |
| Q_{pre-25year} = | 0.89 * 2.1 * 49.13 | 93.54 cfs | |

| 25-Year Post-Development Rainfall Peak Flow | | | |
|---|---------------------------|------------------|--|
| C _w = | 0.72 | | |
| i = | 2.1 in/hr | | |
| A _T = | 49.13 acres | | |
| Q_{post-25year} = | 0.72 * 2.1 * 49.13 | 75.19 cfs | |

CALCULATION OF 100-YEAR PEAK FLOW AND WATER QUALITY FLOW, Q

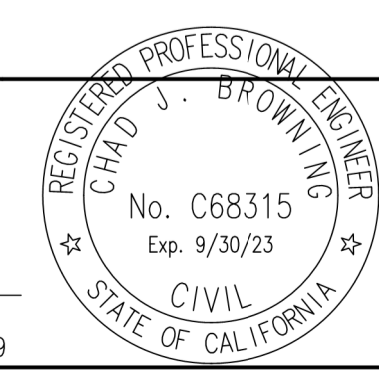
Use the Rational Equation for Peak Flow Calculation:
 $Q = C_w * i * A_T$

- Q = Peak Flow (cfs) for drainage area "A"
- C_w = Weighted runoff coefficient for drainage area A
- i = Intensity (in/hr) based on NOAA's PDS-based precipitation frequency estimates for Cupertino
- A_T = Total Drainage Area (acres)

| 100-Year Pre-Development Rainfall Peak Flow | | | |
|---|---------------------------|-------------------|--|
| C _w = | 0.89 | | |
| i = | 2.7 in/hr | | |
| A _T = | 49.13 acres | | |
| Q_{pre-100year} = | 0.89 * 2.7 * 49.13 | 119.77 cfs | |

| 100-Year Post-Development Rainfall Peak Flow | | | |
|--|---------------------------|------------------|--|
| C _w = | 0.72 | | |
| i = | 2.7 in/hr | | |
| A _T = | 49.13 acres | | |
| Q_{post-100year} = | 0.72 * 2.7 * 49.13 | 96.28 cfs | |

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| No. | REVISION/ISSUE | DATE | BY |
|-------|-------------------------------|------------|----|
| REV-0 | SB-35 DEVELOPMENT APPLICATION | 03/27/2018 | ND |
| REV-1 | SB-35 APPLICATION REVISIONS | 08/06/2018 | ND |
| REV-2 | SB-35 APPLICATION CONFORM SET | 09/15/2018 | ND |
| REV-3 | SB-35 MODIFICATION DOCUMENTS | 03/23/2022 | ND |